Performance Enhancement of Optical Communication Using Decision Feedback Equalization

Amit kaushik¹, Hemant Dalal²
Department of Electronics and Communication^{1,2}
CBS Group of Institutions^{1,2}
Jhajjar, Haryana
Email <u>id-kaushik amit87@yahoo.com</u>, hemantdalal87@gmail.com

Abstract: This paper, proposes an adaptive equalizer by integrating the fractional spaced equalizer (FSE) with decision feedback equalizer (DFE) for optical channel to compensate the problem of pulse dispersion effect in optical link. The performance of the equalizer is improved by adopting the activity detection guidance (ADG) with tap decoupling (TD) in the fractional spaced decision feedback equalizer (FSDFE) to get fruitful outcomes. In this paper a fractionally spaced decision feedback equalization (FSDFE) structure which replaces the symbol spaced feedback filter with a fractionally spaced feedback filter is used to improve the stability and the steady-state error performance and the convergence rate. As the impulse response of a typical optical link would have regions that are essentially zero, the employment of the activity detection scheme with Tap Decoupling would further enhance the steady-state error performance and convergence rate. The simulation results revealed that: the FSDFE with ADG and TD offers a superior performance than its counterpart without ADG and TD. Where, it offers improvement in the effectiveness of amplitude distortion.

Index: ADFE, ADG, DFE, FSE, FSDFE, I.S.I and TD

I. INTRODUCTION

In Long haul optical communications usually there are several keys area to ensure the data transfer is error-free. These areas include modulation method, type of amplifier used, and the error correction scheme and dispersion compensation. In optical communications, high-speed data transfer is limited by signal distortion, caused by the broadening of pulses that result in Intersymbol Interference (ISI).

There are several forms of dispersion, such as: Intermodal dispersion that occurs only in multimode fiber due to different velocities for different modes and hence, it reduces the performance of optical network at higher data rates. The second one is intra-modal dispersion which occurs in all types of fibers. Intramodal dispersion occurs because different colors of light travel through different materials and different waveguide structures at different speeds. Intra modal dispersion is also called as chromatic dispersion (CD) which can be divided into two parts: the first one, is called material dispersion that limits the fiber bandwidth or the information-carrying capacity of the fiber and also limits the transmission distance, since the shorter the pulses, the more susceptible they are to ISI. The second type is the waveguide dispersion occurs because the single-mode fiber only confines about 80 percent of the optical power to the core. Thus dispersion arises due to light propagating in the cladding travels faster than the light confined to the core. So, dispersion occurs because light propagates differently in the core than in the cladding. The intra modal dispersion can be expressed mathematically by

 $\mathbf{D}_{intramodal} = \mathbf{D}_{m} + \mathbf{D}_{WG}$

where: $\mathbf{D}_{\mathbf{M}}$ is the material dispersion, $\mathbf{D}_{\mathbf{WG}}$ is the waveguide dispersion.

The numerous techniques in adaptive equalization and equalizer are used that gives suitable and effective equalization approach for a typical optical channel. In this paper we evaluate the causes of dispersion in a typical optical link and its limiting effects to the possible communication capacity, then to reverse the effects that the channel has on the transmitted signal and reproduce the original signal at the received end. Finally, design an adaptive equalizer to mitigate the pulse dispersion effects of an optical link. A range of adaptive algorithms and equalizer structures are evaluated. The Least Mean Square (LMS) algorithm is chosen for its robustness and computational simplicity.

II. ADAPTIVE EQUALIZER

Linear equalizer is not allways useful for high data bit rate with a dispersive optical channel suffers from ISI or amplitude distortion and used where, the channel does not suffer from amplitude distortion. On the other hand, non-linear equalizer approved its capability to provide superior performance in amplitude distorted channel and will be very beneficial and relevant to the application in optical communications.

The adaptive equalizer is exploited to compensate the dispersion in optical channel, it allows for long haul communication before requiring a repeater, the benefits are to save infrastructure and equipment cost for optical

communication link [1]. It is defined as the equalizer which adjusts to different environments and involves a process of filtering input signal to match a desired response. Its parameters are automatically updated by making a set of measurements of the underlying signals and applying that set to the adaptive filtering algorithm such that the difference between the output and the desired response is minimized in either a statistical or deterministic sense [2]. Concerning the adaptive algorithms, we have several numbers of adaptive algorithms, The most important of them are the least mean squares (LMS) error algorithm and recursive least squares (RLS) algorithm. The criterion used in the adaptive LMS algorithm is the minimization of the mean square error (MSE) between the desired equalizer output and the actual equalizer output in [1 0] for the Ntaps adaptive transversal filter and the output is given by:

$$y(n) = \sum_{i=0}^{N-1} w_i(n) x(n-i)$$

where: x(n-i) is the filter input, $w_i(n)$ is the tap weight.

Fractionally Spaced Equalizer (FSE) is based on sampling the incoming signal at least as fast as the Nyquist rate. Such equalizers have taps that are spaced closer than conventional adaptive equalizers, and with a sufficient number of taps, it is almost independent of the channel delay distortion. It means that the equalizer can negate the channel distortion without enhancing the noise [3]. Given the above properties, the FSE technique is a highly desirable application since it minimizes noise enhancement. With appropriately chosen tap spacing; the FSE can be configured as the excellent feed forward filter. The combination of DFE with FSE technique, provides minimize noise enhancement and Excellent amplitude distortion performance.

Decision Feedback Equalizer

Decision Feedback Equalizer have both the feed forward and feedback filters are essentially linear filters. It is a non-linear structure because of the nonlinear operation in the feedback loop (decision threshold); its current output is based on the output of previous symbols. The decision feedback equalizer has zero noise enhancements in the feedback loop. The above DFE structure has $N_1 + N_2 + 1$ feed forward taps

N₂ feedback taps [2].

The output of the equalizer is given by:

$$d_{k}^{\hat{}} = \sum_{n=N_{i}}^{N_{2}} c_{n}^{*} y_{k-n} \sum_{i=1}^{N_{2}} F_{i} d_{k-i}$$

where is the tap gain and $\mathbf{y} \times \mathbf{n} \ c_{_{_{\mathbf{n}}}}$ is the input for the forward filter, is the tap gain for the feed back filter and dFi x (i<k) is the previous decision made on the detected signal [4].

Activity Detection Guidance

Activity detection guidance technique is a method of detecting active taps in a communication channel, implementing such technique capable of detecting active taps in the channel, non-active taps can be excluded in the estimation of the channel response. This gives a better convergence rate and asymptotic performance. The detection of the 'active' taps of a time-invariant channel is governed by the equation [6]. $c_{k,n} = \frac{(\frac{1}{N} \sum_{i=1}^{N} i u. y_{i-k+1})^2}{\frac{1}{N} \sum_{i=1}^{N} (y_{i-k+1})^2}$

$$c_{k,n} = \frac{(\frac{1}{N}\sum_{i=1}^{N} iu.y_{i-k+1})^2}{\frac{1}{N}\sum_{i=1}^{N} (y_{i-k+1})^2}$$

Where, i is time index, k is tap index, C_{k} is known as the activity measure and N is the number of input samples. In order to determine a tap to be active, the value of the activity measure, C_k, must be above a certain threshold. The activity threshold is given by:

$$C_{K,N} > \sum_{i=1}^{N} \frac{(iu)^2 \cdot \log(i)}{i}$$

Modifications to the activity measure have to be made to reduce the tap coupling effect [6].

$$CC_k = \sum_{i=1}^{N} \frac{\left[(iu - hiu_i + H_k y_{i-k+1}) \cdot (Y_{i-k+1}) \right]^2}{\sum_{i=1}^{N} (Y_{i-k+1})^2}$$

III. Analysis of Impulse Response in Optical Channel

The frequency response of the base band is given by

$$H(f) = \frac{\sin \pi f \tau}{\pi f \tau} \left[\frac{1}{1 - f^2 \tau^2} \right]$$

And the impulse response of a typical optical channel represented by a cosine-squared pulse shape and is given by:

$$h(t) = \begin{cases} \frac{2}{\tau} \cos^2 \frac{\pi t}{\tau}, & -\frac{\tau}{2} \le t \le \frac{\tau}{2} \\ \mathbf{0} & elsewhere \end{cases}$$

SIMULATION RESULTS AND IV. **DISCUSSIONS**

It is clear that the simulated impulse response is resembling a cosine-square shape and having a total of 7-taps. The feed forward section has a total of 6-taps, the fIrst tap has a magnitude of I and the fourth tap has a magnitude of 0.8. The rest of the taps are in active or zero except for tap 7, which is the feedback tap with a magnitude of 1. On the other hand, for the estimated channel impulse response we have run the equalizer for 30000 sample inputs in order to achieve an impulse response in close proximity to the actual simulated

channel. It is clear that the channel bears a fair resemblance of the simulated channel. But, the inactive taps, which were supposed to be zero, were not flat. This is due to the noisy estimates of the inactive taps in the channel.

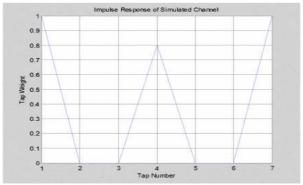


Fig. 1: Impulse response with FSDFE after simulation

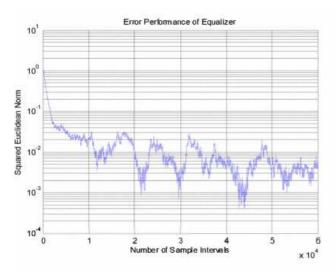


Fig. 3: Asymptotic perfornance for FSDF

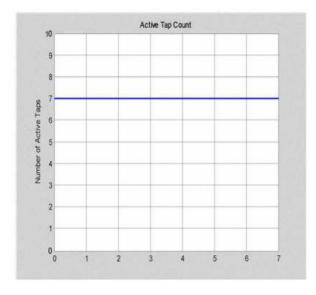


Fig. 4: Active taps count for FSDFE.

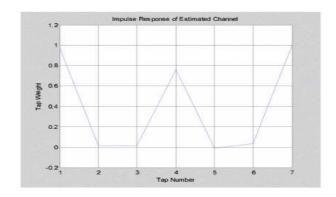


Fig. 2: Estimated channel impulse response for FSDF

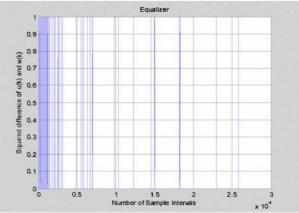


Fig. 5: Squared difference of input to channel and output of equalizer for FSDFE.

FSDFE with ADG and Tap Decoupling.

We have noticed that the inactive taps in the estimated channel were not estimated at zero Adopting ADG with FSDFE could improve the convergence rate and asymptotic performance, detect the non active taps, disregard them in the calculation of the tap weight adoption and set them to zero [5]. However, the true number of active taps cannot be detected accurately and the inactive taps will still suffer from the noisy estimates that are common in any communication channel. The inability to detect the true number of active taps accurately is due to the correlation within the input signal that is causing the coupling amongst the output of the unknown channel taps.

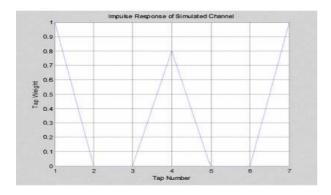


Fig. 6: Simulated channel impulse response.

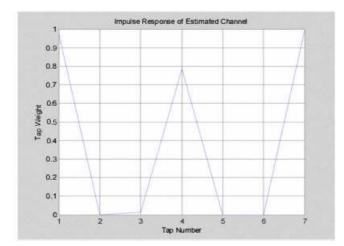


Fig. 7: Estimated channel impulse response.

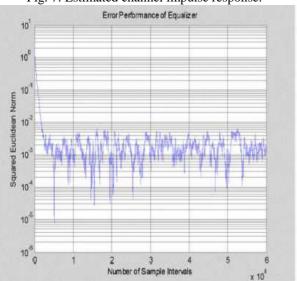


Fig.8: Asymptotic performance of the equalizer.

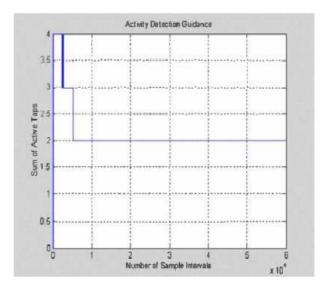


Fig.9: Active taps count.

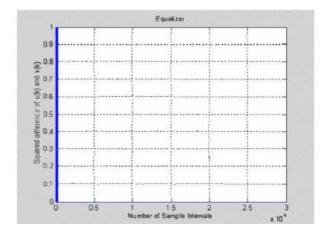


Fig.10: Output of equalizer V. CONCLUSION

With the successful development of the adaptive modified Decision Feedback Equalizer with activity detection guidance and tap decoupling, it offers an excellent alternative to the existing equalization techniques available in the optical communication is implemented using the Least Mean Square (LMS) technique, using stochastic gradient adaptation, led to a faster convergence rate, as only the active taps need to be adapted, and better asymptotic performance as shown clearly.

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